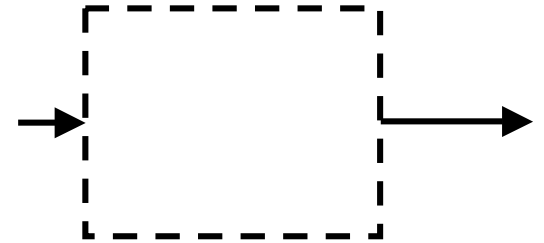


Isentropic Nozzles

- Apply equations for isentropic flow with area change to nozzles

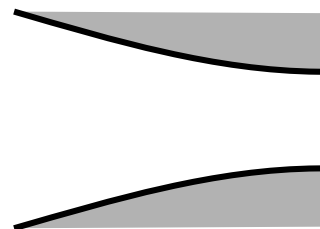
- **Nozzles**

- increases velocity of fluid (no work)
- converts thermal energy to KE ($T \rightarrow u$)



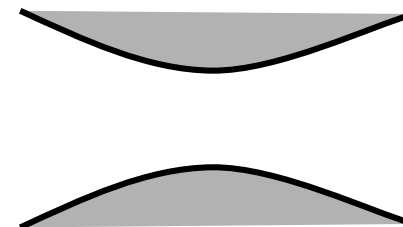
- For conventional (wall-bounded) nozzles, two types:

- converging



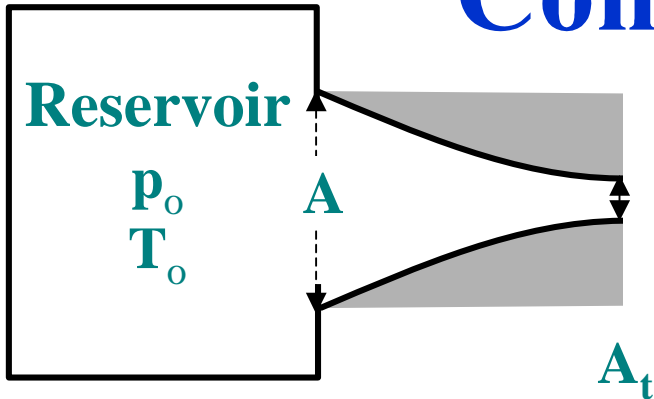
$$M \leq 1$$

- converging-diverging (CD)

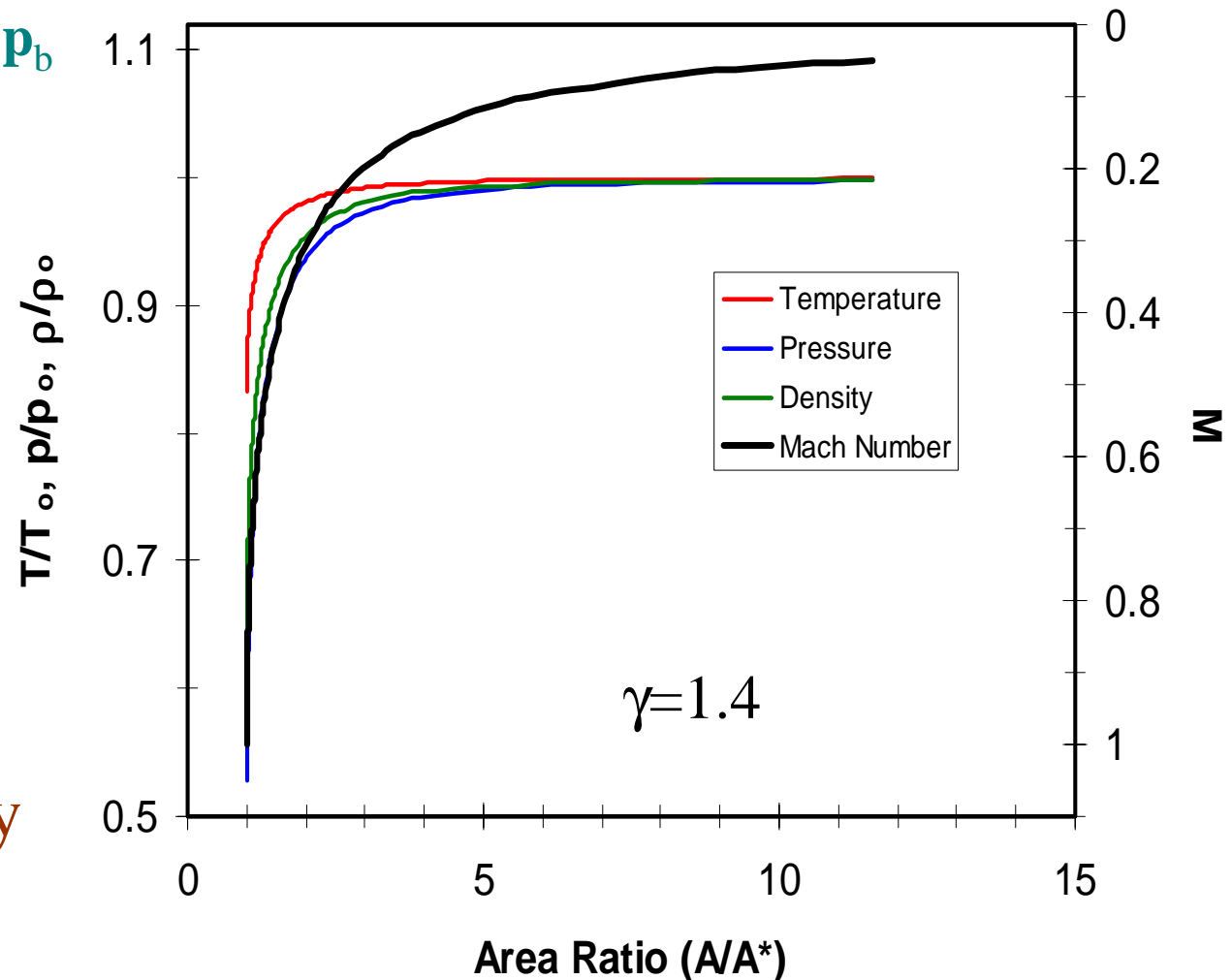


$$0 < M < \infty$$

Converging Nozzles

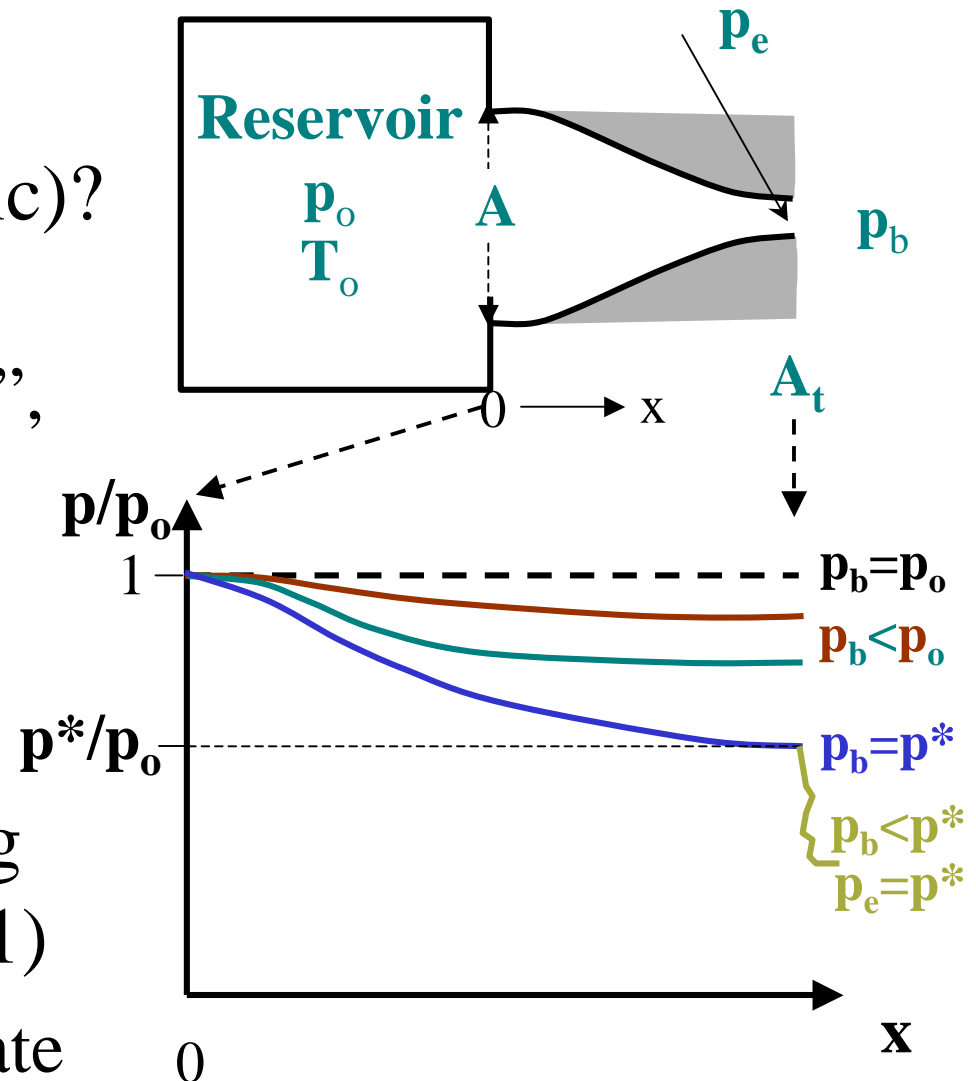


- Assume choked
- Solution of VI.17 (M v. A/A^*)
VI.6-8 (T/T_0 , p/p_0 , ρ/ρ_0 v. M)
- Large change in pressure and density as approach throat



Converging Nozzle and Back Pressure

- What determines whether flow get choked (goes sonic)?
 - **back pressure** (p_o/p_b) pressure is “driving force”, e.g., if $p_o=p_b$, no flow
- What happens as we lower p_b (initially $=p_o$)
- Mach # at exit keeps rising until flow is choked ($M_e=1$)
 - $p_e=p^*$, max. mass flow rate



Critical Back Pressure

- What is p_b/p_o required to go sonic?

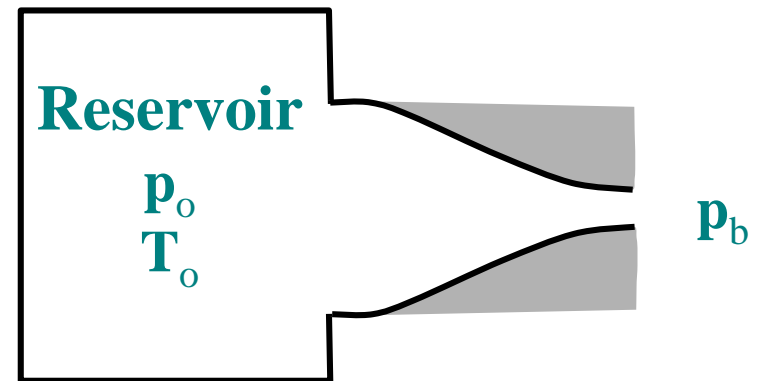
– $p_b/p_o = p^*/p_o$

$$\frac{p_o}{p} = \left(1 + \frac{\gamma-1}{2} M^2 \right)^{\frac{\gamma}{\gamma-1}} \quad (\text{from VI.7})$$

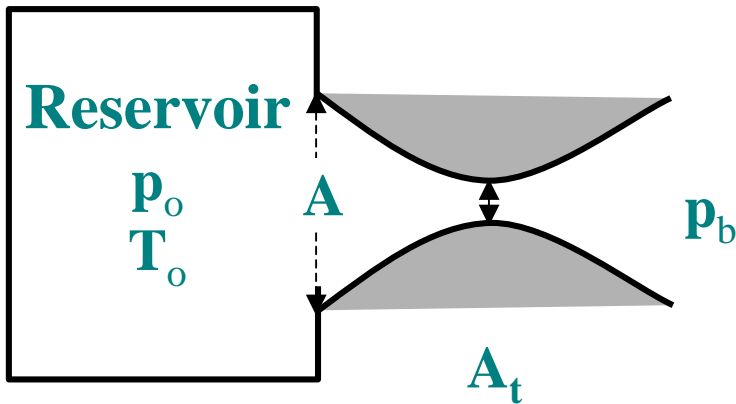
$$\frac{p^*}{p_o} = 1 / \left(1 + \frac{\gamma-1}{2} M^2 \right)^{\frac{\gamma}{\gamma-1}}$$

$$\frac{p^*}{p_o} = \left(\frac{2}{\gamma+1} \right)^{\frac{\gamma}{\gamma-1}} \quad (\text{VI.20})$$

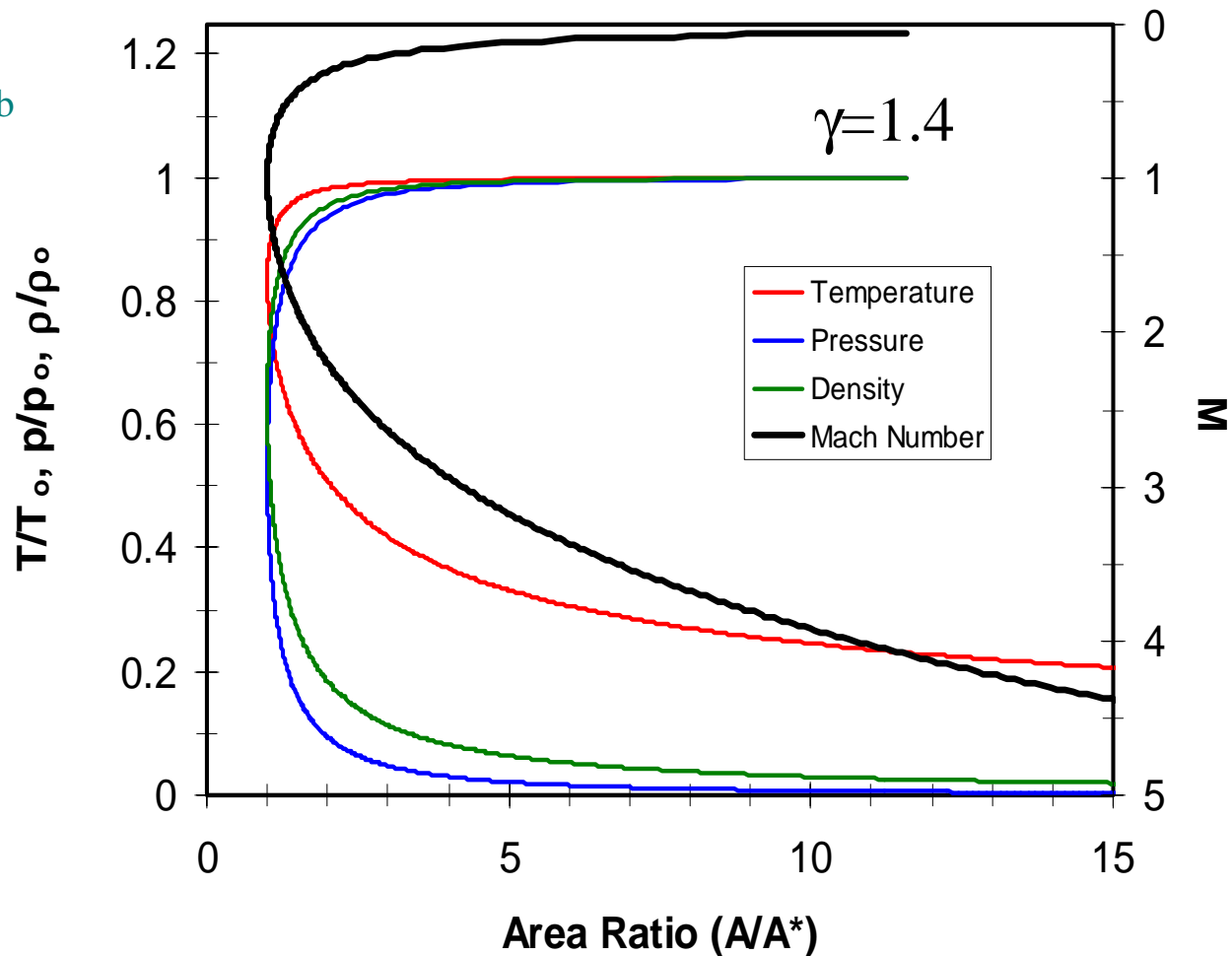
$$= \begin{cases} 0.487 & \gamma = 5/3 \\ 0.528 & \gamma = 1.4 \\ 0.546 & \gamma = 1.3 \end{cases}$$



Converging-Diverging Nozzles



- Assume choked
- Solution of VI.17 (M v. A/A^*)
VI.6-8 (T/T_0 , p/p_0 , ρ/ρ_0 v. M)
- Very large change in pressure and density



CD Nozzle and Back Pressure

- What happens as we lower p_b (initially $=p_o$)?
- M_e keeps rising until flow is choked ($M_t=1$)
 - **still subsonic at exit**
- If lower p_b enough, can get isentropic $M_e > 1$ solution
- p_b in between, get **nonisentropic flow**

