

## Isentropic Nozzles

- Apply equations for isentropic flow with area change to nozzles

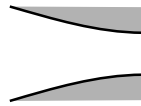
- **Nozzles**

- increases velocity of fluid (no work)
- converts thermal energy to KE ( $T \rightarrow u$ )



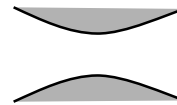
- For conventional (wall-bounded) nozzles, two types:

- converging



$M \leq 1$

- converging-diverging (CD)



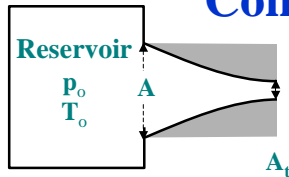
$0 < M < \infty$

Isentropic Nozzles -1

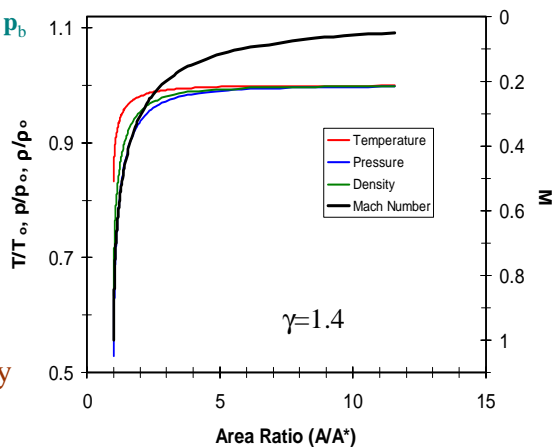
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## Converging Nozzles



- Assume choked
- Solution of VI.17 ( $M$  v.  $A/A^*$ ) VI.6-8 ( $T/T_0$ ,  $p/p_0$ ,  $\rho/\rho_0$  v.  $M$ )
- Large change in pressure and density as approach throat



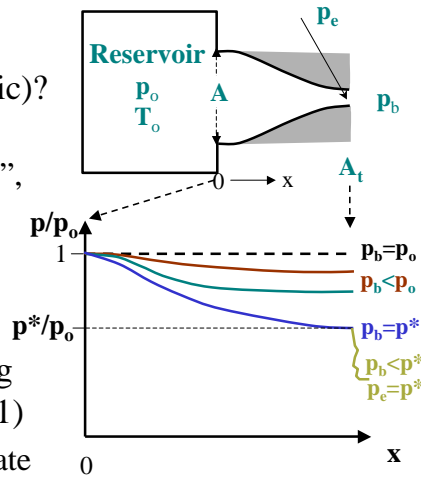
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## Converging Nozzle and Back Pressure

- What determines whether flow get choked (goes sonic)?
  - **back pressure** ( $p_o/p_b$ ) pressure is “driving force”, e.g., if  $p_o=p_b$ , no flow
- What happens as we lower  $p_b$  (initially  $=p_o$ )
- Mach # at exit keeps rising until flow is choked ( $M_e=1$ )
  - $p_e=p^*$ , max. mass flow rate



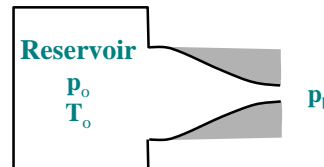
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## Critical Back Pressure

- What is  $p_b/p_o$  required to go sonic?
  - $p_b/p_o = p^*/p_o$



$$\frac{p_o}{p} = \left(1 + \frac{\gamma-1}{2} M^2\right)^{\gamma/\gamma-1} \quad (\text{from VI.7})$$

$$\frac{p^*}{p_o} = 1 / \left(1 + \frac{\gamma-1}{2} 1^2\right)^{\gamma/\gamma-1}$$

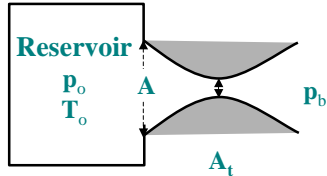
$$\frac{p^*}{p_o} = \left(\frac{2}{\gamma+1}\right)^{\gamma/\gamma-1} \quad (\text{VI.20}) = \begin{cases} 0.487 & \gamma = 5/3 \\ 0.528 & \gamma = 1.4 \\ 0.546 & \gamma = 1.3 \end{cases}$$

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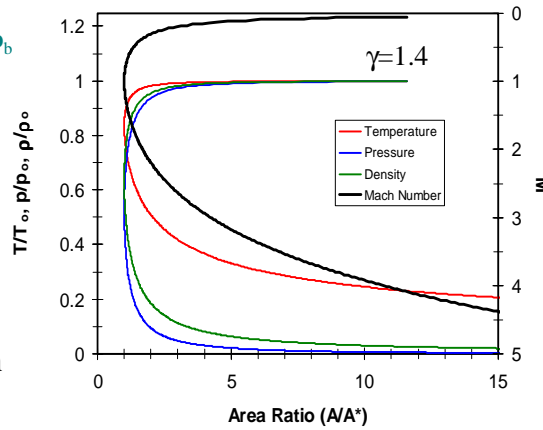
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## Converging-Diverging Nozzles



- Assume choked
- Solution of VI.17 ( $M \cdot v \cdot A/A^*$ ) VI.6-8 ( $T/T_0, p/p_0, \rho/\rho_0 \cdot v \cdot M$ )
- Very large change in pressure and density



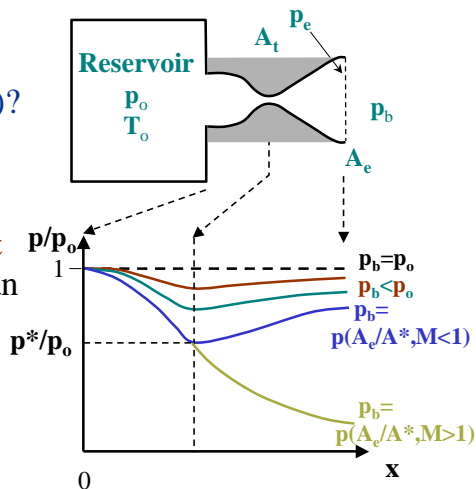
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## CD Nozzle and Back Pressure

- What happens as we lower  $p_b$  (initially  $=p_0$ )?
- $M_e$  keeps rising until flow is choked ( $M_t=1$ )
  - still subsonic at exit
- If lower  $p_b$  enough, can get isentropic  $M_e > 1$  solution
- $p_b$  in between, get nonisentropic flow



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