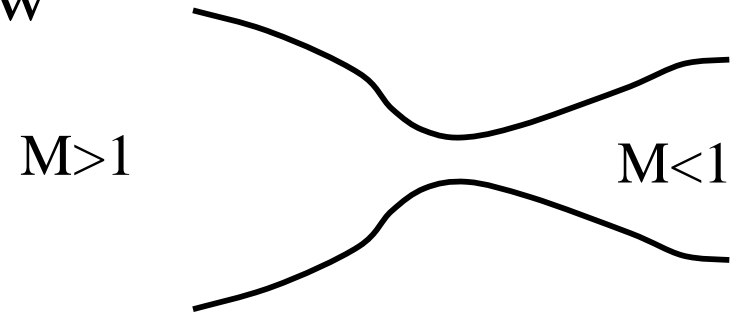


# Supersonic (Engine) Inlets

- For air-breathing engines on supersonic vehicles, usually want to slow flow down to subsonic speeds inside engine
  - need diffuser ( $M > 1 \rightarrow M < 1$ ) for engine inlet
  - exception: supersonic combustion (e.g., SCRAM jets)
- Goal
  - lowest  $p_o$  loss (highest thrust)
    - given flight  $M$
    - mass flow rate requirement (thrust)
    - stable operation (nothing drastic for small changes in flight conditions)

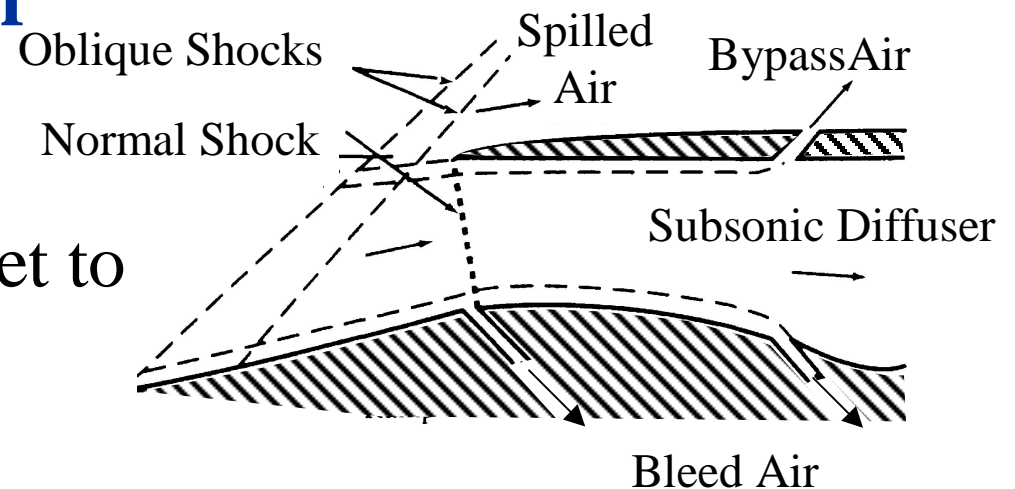
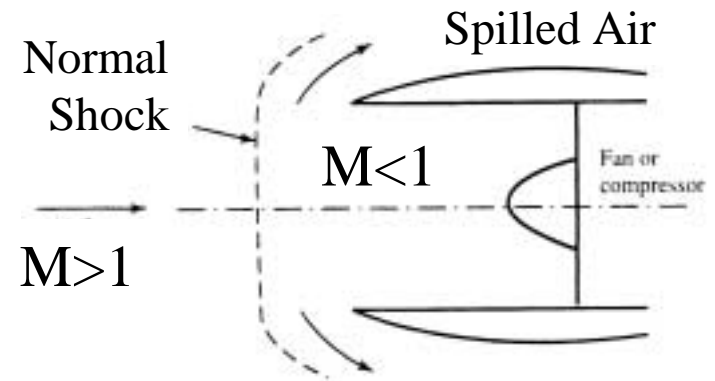
# CD Inlet

- Can get close to isentropic flow
  - lowest potential  $p_o$  loss
  - starting problem  
(like supersonic wind tunnel, have to swallow shock)
  - most cases requires **variable area throat** (heavy, complex)
  - **stability problem**: if “shock” leaves throat, can exit engine lowering mass flow (higher  $A_2^*$ )
- **Not typically used**



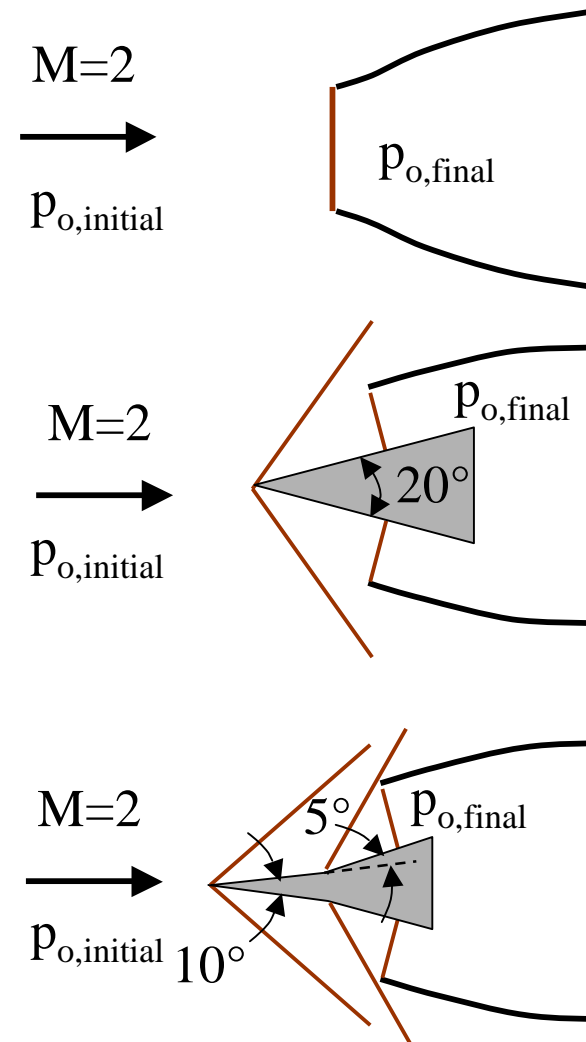
# Shock Inlets

- Normal shock diffuser**
  - simple, diverging section preceded by normal shock
  - highest  $p_o$  loss (strong shock)
- Oblique Shock Diffuser**
  - oblique shock(s) followed by normal shock at (or inside) inlet to subsonic diffuser
  - lower  $p_o$  loss
  - works for range of  $M$



# Example: Normal v. Oblique Diffusers

- **Given:** You need to pick a diffuser for Mach 2 flight conditions. Your choices are a normal shock diffuser and 2 different oblique shock diffusers
- **Find:** Stagnation pressure loss for each ( $p_{o,final}/p_{o,initial}$ )
- **Assume:** air is TPG/CPG with  $\gamma=1.4$ , steady, adiabatic, no work, inviscid except for shock,....



# Solution: Normal v. Oblique Diffusers

- **Analysis:**

- **Normal Shock Diffuser**

Table B.1 or VI.31,33

$$M_1 = 2 \Rightarrow M_2 = 0.577, p_{o2}/p_{o1} = 0.721$$

- **Single Oblique Shock (+Normal)**

VI.46 or C.1

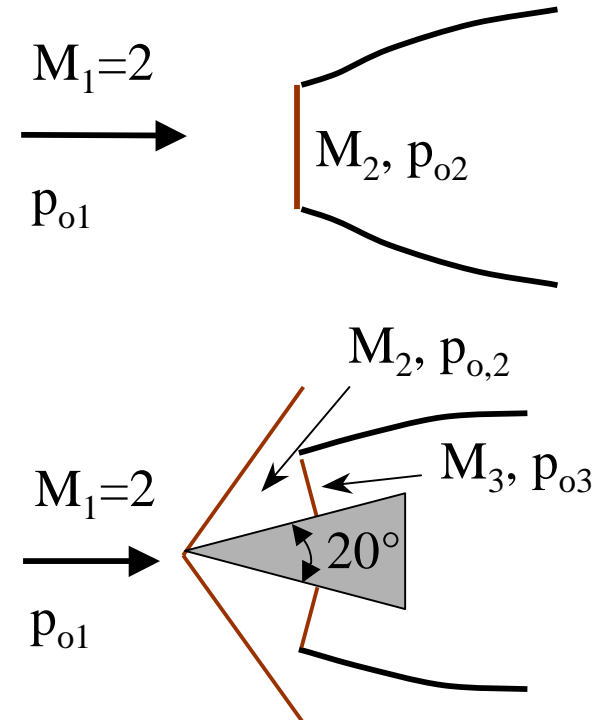
$$M_1 = 2, \delta = 10^\circ \Rightarrow \theta = 39.3^\circ$$

$$M_{1n} = M_1 \sin \theta = 2 \sin 39.3^\circ = 1.267$$

$$\text{B.1 or VI.31,33} \Rightarrow M_{2n} = 0.803; p_{o2}/p_{o1} = 0.985$$

$$M_2 = M_{2n} / \sin(\theta - \delta) = 1.64$$

$$\text{B.1 or VI.31,33} \Rightarrow M_3 = 0.657; p_{o3}/p_{o2} = 0.880$$



$$\frac{p_{o3}}{p_{o1}} = \frac{p_{o3}}{p_{o2}} \frac{p_{o2}}{p_{o1}} = 0.867$$

normal shock inlet - 28%  $p_o$  loss  
 oblique shock inlet - 13.3%  $p_o$  !!!

# Solution: Normal v. Oblique Diffusers

- Analysis: (con't)

- Two 5° Turns (+Normal Shock)

VI.46 or C.1

$$M_1 = 2, \delta_1 = 5^\circ \Rightarrow \theta_1 = 34.3^\circ$$

$$M_{1n} = M_1 \sin \theta_1 = 2 \sin 34.3^\circ = 1.127$$

B.1 or VI.31,33  $\Rightarrow M_{2n} = 0.891; p_{o2}/p_{o1} = 0.998$

$$M_2 = M_{2n} / \sin(\theta_1 - \delta_1) = 1.82$$

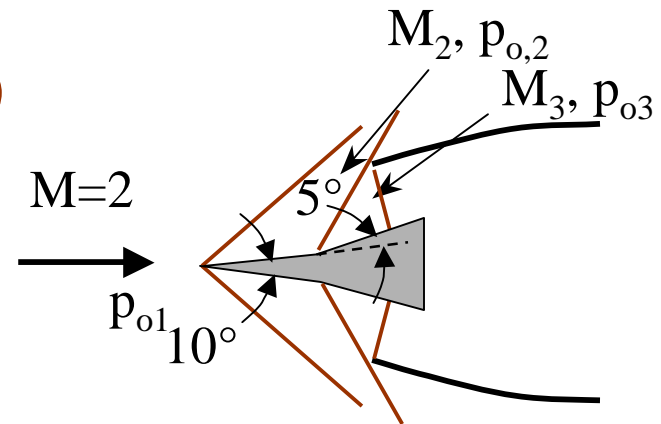
VI.46 or C.1  $M_2 = 1.82, \delta_2 = 5^\circ \Rightarrow \theta_2 = 37.9^\circ$

$$M_{2n} = M_2 \sin \theta_2 = 1.82 \sin 38.0^\circ = 1.120$$

B.1 or VI.31,33  $\Rightarrow M_{3n} = 0.897; p_{o2}/p_{o1} = 0.998$

$$M_3 = M_{3n} / \sin(\theta_2 - \delta_2) = 1.65$$

B.1 or VI.31,33  $\Rightarrow M_3 = 0.654; p_{o4}/p_{o3} = 0.8765$



$$\frac{p_{o4}}{p_{o1}} = \frac{p_{o4}}{p_{o3}} \frac{p_{o3}}{p_{o2}} \frac{p_{o2}}{p_{o1}} = 0.873$$

double obl. shock inlet  
~ 12.7%  $p_o$  loss

# Double Oblique Inlet - Advantages

- So for  $M=2$ , same total turning angle ( $10^\circ$ )
  - **two oblique shocks** slightly better than one (12.7% v. 13.3%  $p_o$  loss )
  - significant improvement over normal shock alone (28%  $p_o$  loss)
- Oblique shock diffuser with two  $10^\circ$  turns (total  $\delta$  of  $20^\circ$ ) even better
  - only 4.3%  $p_o$  loss (solution shown on next slide)
  - so **larger overall deflection can give better  $p_o$**
- Stagnation pressure advantages of using multiple oblique shocks increase with higher  $M$

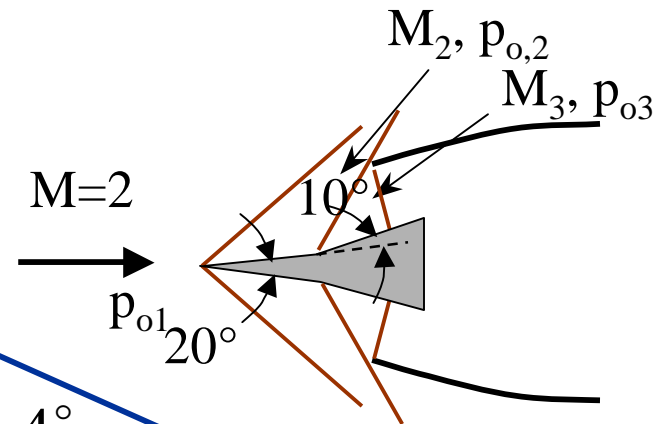
# Double Oblique Shock Diffuser

- **Two 10° Turns (+Normal Shock)**

from previous results for 10° turn

$$M_1 = 2, \delta = 10^\circ \Rightarrow \theta_1 = 34.3^\circ$$

$$M_2 = 1.64; p_{o2}/p_{o1} = 0.985$$



VI.46 or C.1  $M_2 = 1.64, \delta_2 = 10^\circ \Rightarrow \theta_2 = 49.4^\circ$

$$M_{2n} = M_2 \sin \theta_2 = 1.64 \sin 49.4^\circ = 1.245$$

B.1 or VI.31,33  $\Rightarrow M_{3n} = 0.815; p_{o2}/p_{o1} = 0.988$

$$M_3 = M_{3n} / \sin(\theta_2 - \delta_2) = 1.28$$

B.1 or VI.31,33  $\Rightarrow M_4 = 0.796; p_{o4}/p_{o3} = 0.983$

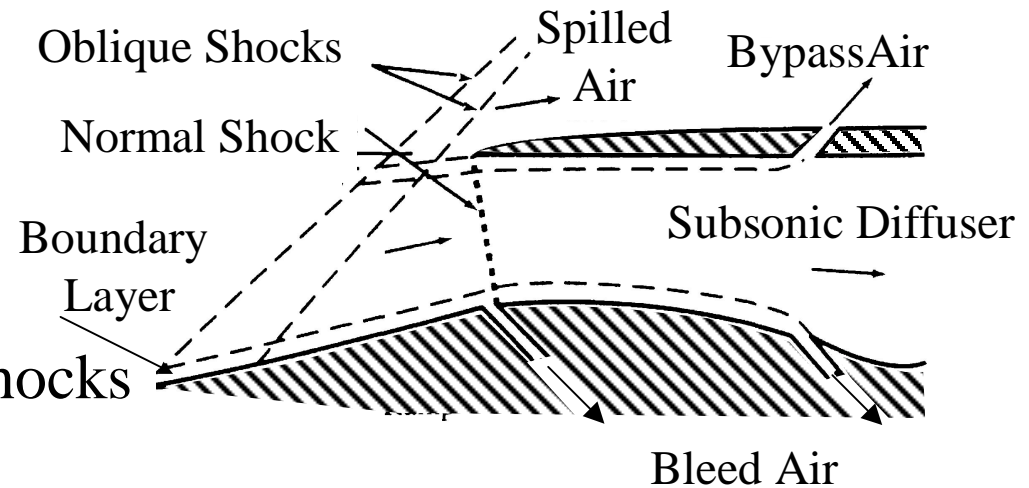
$$\begin{aligned}
 \frac{p_{o4}}{p_{o1}} &= \frac{p_{o4}}{p_{o3}} \frac{p_{o3}}{p_{o2}} \frac{p_{o2}}{p_{o1}} \\
 &= 0.957
 \end{aligned}$$



# Double Oblique Inlet - Disadvantages

- **Flow separation**

- since  $p$  increases across oblique shocks, the flow sees adverse  $p$  gradient
- so more or bigger oblique shocks (or longer external ramp), the greater the chance the boundary layer will separate
  - ⇒ major change in flowfield, large losses ( $p_o$  and mass flowrate)



- **Internal Turn Angle**

- larger total external turn angle showed less  $p_o$  loss
- larger external flow turning requires larger inlet
- also requires larger internal flow turning to get flow back to horizontal