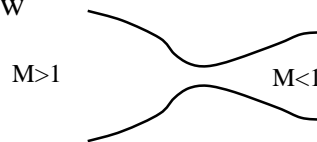


Supersonic (Engine) Inlets

- For air-breathing engines on supersonic vehicles, usually want to slow flow down to subsonic speeds inside engine
 - need diffuser ($M > 1 \rightarrow M < 1$) for engine inlet
 - exception: supersonic combustion (e.g., SCRAM jets)
- Goal
 - lowest p_o loss (highest thrust)
 - given flight M
 - mass flow rate requirement (thrust)
 - stable operation (nothing drastic for small changes in flight conditions)

CD Inlet

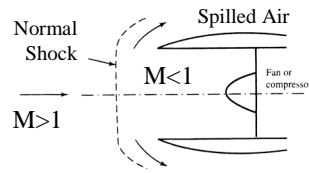
- Can get close to isentropic flow
 - lowest potential p_o loss
 - starting problem (like supersonic wind tunnel, have to swallow shock)
 - most cases requires variable area throat (heavy, complex)
 - stability problem: if “shock” leaves throat, can exit engine lowering mass flow (higher A_2^*)
- **Not typically used**



Shock Inlets

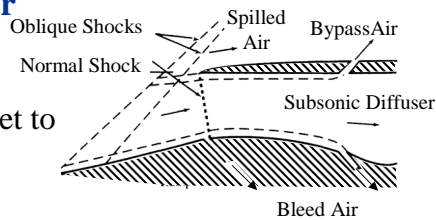
- **Normal shock diffuser**

- simple, diverging section preceded by normal shock
- highest p_o loss (strong shock)



- **Oblique Shock Diffuser**

- oblique shock(s) followed by normal shock at (or inside) inlet to subsonic diffuser
- lower p_o loss
- works for range of M

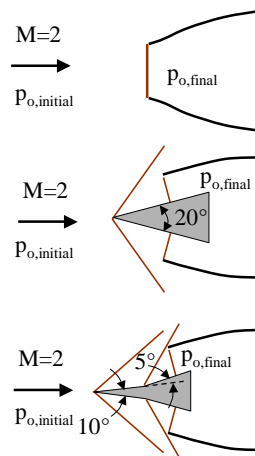


Supersonic Inlets - Oblique Shocks - 3
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Example: Normal v. Oblique Diffusers

- **Given:** You need to pick a diffuser for Mach 2 flight conditions. Your choices are a normal shock diffuser and 2 different oblique shock diffusers
- **Find:** Stagnation pressure loss for each ($p_{o,final}/p_{o,initial}$)
- **Assume:** air is TPG/CPG with $\gamma=1.4$, steady, adiabatic, no work, inviscid except for shock,....



Supersonic Inlets - Oblique Shocks - 4
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Solution: Normal v. Oblique Diffusers

• Analysis:

– Normal Shock Diffuser

Table B.1 or VII.11,13

$$M_1 = 2 \Rightarrow M_2 = 0.577, p_{o2}/p_{o1} = 0.721$$

– Single Oblique Shock (+Normal)

VII.26 or C.1

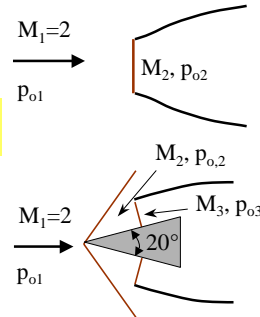
$$M_1 = 2, \delta = 10^\circ \Rightarrow \theta = 39.3^\circ$$

$$M_{1n} = M_1 \sin \theta = 2 \sin 39.3^\circ = 1.267$$

$$\text{B.1 or VII.11,13} \Rightarrow M_{2n} = 0.803; p_{o2}/p_{o1} = 0.985$$

$$M_2 = M_{2n} / \sin(\theta - \delta) = 1.64$$

$$\text{B.1 or VII.11,13} \Rightarrow M_3 = 0.657; p_{o3}/p_{o2} = 0.880$$



$$\frac{p_{o3}}{p_{o1}} = \frac{p_{o3}}{p_{o2}} \frac{p_{o2}}{p_{o1}} = 0.867$$

normal shock inlet - 28% p_o loss
oblique shock inlet - 13.3% p_o !!!

Solution: Normal v. Oblique Diffusers

• Analysis: (con't)

– Two 5° Turns (+Normal Shock)

VII.26 or C.1

$$M_1 = 2, \delta_1 = 5^\circ \Rightarrow \theta_1 = 34.3^\circ$$

$$M_{1n} = M_1 \sin \theta_1 = 2 \sin 34.3^\circ = 1.127$$

$$\text{B.1 or VII.11,13} \Rightarrow M_{2n} = 0.891; p_{o2}/p_{o1} = 0.998$$

$$M_2 = M_{2n} / \sin(\theta_1 - \delta_1) = 1.82$$

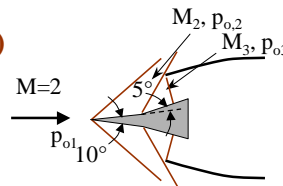
$$\text{VII.26 or C.1} M_2 = 1.82, \delta_2 = 5^\circ \Rightarrow \theta_2 = 37.9^\circ$$

$$M_{2n} = M_2 \sin \theta_2 = 1.82 \sin 38.0^\circ = 1.120$$

$$\text{B.1 or VII.11,13} \Rightarrow M_{3n} = 0.897; p_{o2}/p_{o1} = 0.998$$

$$M_3 = M_{3n} / \sin(\theta_2 - \delta_2) = 1.65$$

$$\text{B.1 or VII.11,13} \Rightarrow M_4 = 0.654; p_{o4}/p_{o3} = 0.8765$$



$$\frac{p_{o4}}{p_{o1}} = \frac{p_{o4}}{p_{o3}} \frac{p_{o3}}{p_{o2}} \frac{p_{o2}}{p_{o1}} = 0.873$$

double obl. shock inlet
~ 12.7% p_o loss

Double Oblique Inlet - Advantages

- So for $M=2$, same total turning angle (10°)
 - two oblique shocks slightly better than one (12.7% v. 13.3% p_o loss)
 - significant improvement over normal shock alone (28% p_o loss)
- Oblique shock diffuser with two 10° turns (total δ of 20°) even better
 - only 4.3% p_o loss (solution shown on next slide)
 - so larger overall deflection can give better p_o
- Stagnation pressure advantages of using multiple oblique shocks increase with higher M

Double Oblique Shock Diffuser

- Two 10° Turns (+Normal Shock)

from previous results for 10° turn

$$M_1 = 2, \delta = 10^\circ \Rightarrow \theta_1 = 34.3^\circ$$

$$M_2 = 1.64; p_{o2}/p_{o1} = 0.985$$

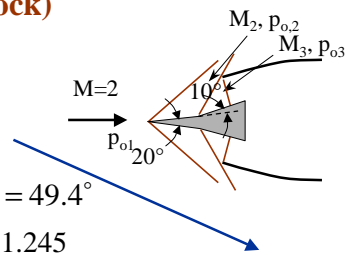
$$\text{VII.26 or C.1} M_2 = 1.64, \delta_2 = 10^\circ \Rightarrow \theta_2 = 49.4^\circ$$

$$M_{2n} = M_2 \sin \theta_2 = 1.64 \sin 49.4^\circ = 1.245$$

$$\text{B.1 or VII.11,13} \Rightarrow M_{3n} = 0.815; p_{o2}/p_{o1} = 0.988$$

$$M_3 = M_{3n} / \sin(\theta_2 - \delta_2) = 1.28$$

$$\text{B.1 or VII.11,13} \Rightarrow M_3 = 0.796; p_{o4}/p_{o3} = 0.983$$

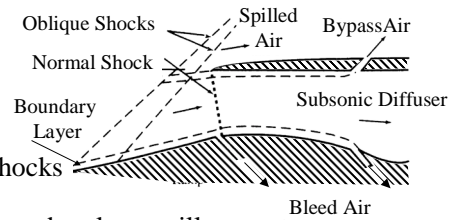


$$\frac{p_{o4}}{p_{o1}} = \frac{p_{o4}}{p_{o3}} \frac{p_{o3}}{p_{o2}} \frac{p_{o2}}{p_{o1}} = 0.957$$

Double Oblique Inlet - Disadvantages

- **Flow separation**

- since p increases across oblique shocks, the flow sees adverse p gradient
- so more or bigger oblique shocks (or longer external ramp), the greater the chance the boundary layer will separate
⇒ major change in flowfield, large losses (p_0 and mass flowrate)



- **Internal Turn Angle**

- larger total external turn angle showed less p_0 loss
- larger external flow turning requires larger inlet
- also requires larger internal flow turning to get flow back to horizontal