

T Dependence of Equilibrium Constant

- **Basic issue**

- we know K_p that (or K_c , K_f), for a given *reaction expression*, is function of temperature only, $K_p = K_p(T)$
- can we describe/model its temperature dependence (for a TPG)

- **Approach**

- employ previously derived expressions relating Gibbs Free Energy and Enthalpy (van't Hoff)

$$\left. \frac{\partial(G/T)}{\partial T} \right|_{p, n_i} = \frac{-H}{T^2} \quad \text{and for TPG} \quad \frac{d(\mu_i^\circ/T)}{dT} = \frac{-\bar{h}_i}{T^2} = \frac{-\hat{h}_i}{T^2}$$

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van't Hoff's Equation

- Start with K_p “definition” (TPG)

$$\ln K_p = \frac{-1}{RT} \sum_i \nu_i \mu_i^\circ = \frac{-1}{R} \sum_i \nu_i \frac{\mu_i^\circ}{T}$$

- Get T dependence from derivative

$$\frac{d}{dT} (\ln K_p) = \frac{d}{dT} \left(\frac{-1}{R} \sum_i \nu_i \frac{\mu_i^\circ}{T} \right) = \frac{-1}{R} \sum_i \nu_i \frac{d}{dT} \left(\frac{\mu_i^\circ}{T} \right)$$

$$= \frac{1}{R} \sum_i \nu_i \frac{\hat{h}_i}{T^2}$$

$$\sum_i \nu_i \hat{h}_i = ?$$

$$= \hat{H}_{RHS}^\circ - \hat{H}_{LHS}^\circ \equiv \Delta \hat{H}_R^\circ \quad \text{Standard Heat of Reaction}$$

$$\Delta \hat{H}_R \begin{cases} < 0 & \text{Exothermic} \\ > 0 & \text{Endothermic} \end{cases}$$

drop ° since TPG $H \neq \hat{H}(p)$

$$\frac{d \ln K_p}{dT} = \frac{\Delta \hat{H}_R(T)}{RT^2}$$

van't Hoff's Eq'n.

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K_p Temperature Dependence

$$\frac{d}{dT}(\ln K_p) = \frac{\Delta \hat{H}_R(T)}{RT^2} \begin{cases} < 0 & \text{exothermic} \\ > 0 & \text{endothermic} \end{cases}$$

- Integrating gives $K_p(T)$ from H data, but 1st, how to interpret this expression?
- From K_p def'n.
$$K_p = \frac{\prod_i \chi_{i,RHS}^{|\nu_i|}}{\prod_i \chi_{i,LHS}^{|\nu_i|}} p^{\Delta n_R} \quad \Delta n_R \equiv \sum_i \nu_i$$
 - for exothermic expression: $T \uparrow \Rightarrow K_p \downarrow$ (more LHS)
 - for endothermic expression: $T \uparrow \Rightarrow K_p \uparrow$ (more RHS)
- Recall p dependence
 - $p \uparrow \Rightarrow$ more lower moles side

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Interpolating for K_p

$$\frac{d \ln K_p}{dT} = \frac{\Delta \hat{H}_R(T)}{RT^2} \Rightarrow \int_{K_{p1}}^{K_{p2}} d \ln K_p = \ln \frac{K_{p2}}{K_{p1}} = \int_{T_1}^{T_2} \frac{\Delta \hat{H}_R(T)}{RT^2} dT$$

- Can use this to find $K_p(T_2)$ if $K_p(T_1)$ known -- if we have information (e.g. tables) on heat of reaction
- For “small” ΔT , assume $\Delta \hat{H}_R \sim \text{constant}$

$$\ln \frac{K_{p2}}{K_{p1}} \approx \frac{\Delta \hat{H}_R(T_1)}{R} \left[\frac{1}{T_1} - \frac{1}{T_2} \right]$$

“small” ΔT when change in 2nd term below is “small” – so better when strongly exothermic or endothermic
- Otherwise

$$\begin{aligned} \Delta \hat{H}_R &= \sum \nu_i \hat{h}_i = \sum \nu_i \left(\hat{h}_{i,0} + \int_0^T \hat{c}_{p_i} dT \right) \cong \Delta \hat{H}_{R,0} + \sum \nu_i \int_0^T (a_i + b_i T + c_i T^2) dT \\ &\cong \Delta \hat{H}_{R,0} + \sum \nu_i \left(a_i T + \frac{1}{2} b_i T^2 + \frac{1}{3} c_i T^3 \right) \\ \ln K_p &\cong C + \frac{1}{R} \left\{ -\Delta \hat{H}_{R,T=0}/T + \sum \nu_i (a_i \ln T + b_i T/2 + c_i T^2/6) \right\} \end{aligned}$$

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K_c Temperature Dependence

- For TPG, we had

$$\begin{aligned}\ln K_c &= \ln K_p - \ln(\bar{R}T)^{\sum \nu_i} = \ln K_p - \Delta n_R \ln(\bar{R}T) \\ \frac{d}{dT} \ln K_c &= \frac{d}{dT} \ln K_p - \Delta n_R \frac{d}{dT} \ln(\bar{R}T) = \frac{\Delta \hat{H}_R}{\bar{R}T^2} - \Delta n_R \frac{1}{T} \\ &= \frac{\Delta \hat{H}_R - \Delta n_R \bar{R}T}{\bar{R}T^2} \\ pV &= n\bar{R}T \Rightarrow \Delta(pV)_{\text{fixed } T} = (\Delta n)\bar{R}T \\ &= \frac{\Delta \hat{H}_R - \Delta pV}{\bar{R}T^2} \\ \boxed{\frac{d}{dT} \ln K_c = \frac{\Delta \hat{U}_R}{\bar{R}T^2}}\end{aligned}$$

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K_f Temperature Dependence

- Using similar approach for imperfect gases

$$\frac{d}{dT} \ln K_f = \frac{\sum \nu_i \hat{h}_i^o}{\bar{R}T^2}$$

- Pick f^o condition at low enough p such that $f^o/p^o=1$
 - we can choose any ref. (o) condition we want
 - by choosing low pressure \Rightarrow TPG and $\bar{h}_i = \hat{h}_i$
and since K_f not function of f

$$\frac{d}{dT} \ln K_f = \frac{\Delta \hat{H}_R^o}{\bar{R}T^2}$$

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